

## Technical Notes

### The Inverse Problem for a Finite Slab

C. E. Siewert\*

*Centre d'Etudes Nucléaires de Saclay  
Division d'Etude et de Développement des Réacteurs  
B.P. 2, 91190 Gif-sur-Yvette, France*

*Received October 5, 1977*

*Accepted February 23, 1978*

#### ABSTRACT

*The finite-slab inverse problem for multigroup neutron transport theory is solved.*

#### INTRODUCTION

In a recent Note,<sup>1</sup> the inverse problem for multigroup transport theory was discussed and solved for an infinite medium. Here we solve the inverse problem for the considerably more important case of a finite slab.<sup>2</sup> Traditionally, we seek to determine the angular flux after specifying the physical parameters of the medium and

---

\*Permanent address: North Carolina State University, Nuclear Engineering Department, Raleigh, North Carolina 27607.

<sup>1</sup>C. E. SIEWERT, M. N. ÖZİŞİK, and Y. YENER, *Nucl. Sci. Eng.*, **63**, 95 (1977).

<sup>2</sup>S. PAHOR, *Phys. Rev.*, **175**, 218 (1968).

appropriate boundary conditions. For the inverse problem, we wish to determine the physical parameters from a measurement of the flux and the angular distribution of neutrons leaving the slab.

### ANALYSIS

We consider a finite subcritical medium defined by

$$\begin{aligned} \mu \frac{\partial}{\partial x} \Psi(x, \mu) + \Sigma \Psi(x, \mu) \\ = \sum_{l=0}^{\infty} \left( \frac{2l+1}{2} \right) P_l(\mu) \mathbf{C}_l \int_{-1}^1 \Psi(x, \mu') P_l(\mu') d\mu' , \\ x \in [0, a] . \end{aligned} \quad (1)$$

Here  $\Psi(x, \mu)$  is an  $n \times n$  matrix, the columns of which are the angular fluxes,  $\Sigma$  is the diagonal total cross-section matrix, and the elements of the transfer matrices  $\mathbf{C}_l$  are the  $l$ 'th angular components of the transfer cross sections for fission and scattering. Since we allow  $\Psi(x, \mu)$  to be an  $n \times n$  matrix, we consider boundary conditions of the form

$$\Psi(0, \mu) = \mathbf{F}(\mu) , \quad \mu > 0 , \quad (2a)$$

and

$$\Psi(a, -\mu) = \mathbf{0} , \quad \mu > 0 , \quad (2b)$$

where  $\mathbf{F}(\mu)$  is an  $n \times n$  matrix that we consider to be specified. We note that the  $\alpha$ 'th column of  $\Psi(x, \mu)$  is the angular flux vector corresponding to an incident distribution represented by the  $\alpha$ 'th column of  $\mathbf{F}(\mu)$ .

If we multiply Eq. (1) by  $P_l(\mu)$  and integrate over  $\mu$ , we find

$$(2l+1) \Delta_l \Psi_l(x) = -(l+1) \Psi'_{l+1}(x) - l \Psi'_{l-1}(x) , \quad (3)$$

where

$$\Delta_l = \Sigma - \mathbf{C}_l \quad (4)$$

and

$$\Psi_l(x) = \int_{-1}^1 P_l(\mu) \Psi(x, \mu) d\mu . \quad (5)$$

If we multiply Eq. (3), for  $l=0$ , by  $x^\alpha$ ,  $\alpha=0, 1, 2, 3, \dots$ , and integrate over  $x$ , we can write

$$\Delta_0 \int_0^a x^\alpha \Psi_0(x) dx = \delta_{\alpha,0} \Psi_1(0) - a^\alpha \Psi_1(a) + \alpha \int_0^a x^{\alpha-1} \Psi_1(x) dx , \quad (6)$$

which, for  $\alpha=0$ , yields

$$\Delta_0^{-1} = \mathbf{M}_0 [\Psi_1(0) - \Psi_1(a)]^{-1} , \quad (7)$$

where

$$\mathbf{M}_\alpha = \int_0^a x^\alpha \Psi_0(x) dx . \quad (8)$$

From Eq. (3), we see that

$$\Psi_1(x) = -\frac{1}{3} \Delta_1^{-1} [2\Psi_2'(x) + \Psi_0'(x)] , \quad (9)$$

which can be used in Eq. (6) to obtain

$$\begin{aligned} \Delta_0 \mathbf{M}_\alpha - \frac{1}{3} \alpha(\alpha-1) \Delta_1^{-1} \mathbf{M}_{\alpha-2} + a^\alpha \Psi_1(a) - \frac{1}{3} \alpha \Delta_1^{-1} \\ \times \{ \delta_{\alpha,1} [2\Psi_2(0) + \Psi_0(0)] - a^{\alpha-1} [2\Psi_2(a) + \Psi_0(a)] \} \\ = \frac{2}{3} \alpha(\alpha-1) \Delta_1^{-1} \int_0^a x^{\alpha-2} \Psi_2(x) dx , \quad \alpha \geq 1 . \end{aligned} \quad (10)$$

We can solve Eq. (10) for  $\alpha=1$  to obtain

$$\Delta_1^{-1} = 3 [\Delta_0 \mathbf{M}_1 + a \Psi_1(a)] \{ 2[\Psi_2(0) - \Psi_2(a)] + \Psi_0(0) - \Psi_0(a) \}^{-1} . \quad (11)$$

It is clear that we can continue to use Eq. (3) in Eq. (10) and to integrate by parts to find all of the  $\Delta_l$  in terms of spatial moments of the flux  $\mathbf{M}_\alpha$  and angular moments of the reflected and transmitted angular fluxes,  $\Psi_l(0)$  and  $\Psi_l(a)$ . We list the following explicit results:

$$\Delta_0^{-1} = \mathbf{M}_0 \mathbf{N}_0^{-1} , \quad (12a)$$

$$\Delta_1^{-1} = 3 [\Delta_0 \mathbf{M}_1 + a \Psi_1(a)] \mathbf{N}_1^{-1} , \quad (12b)$$

$$\begin{aligned} \Delta_2^{-1} = \left\{ \frac{15}{4} \Delta_1 \Delta_0 \mathbf{M}_2 - \frac{5}{2} \mathbf{M}_0 + \frac{15}{4} a^2 \Delta_1 \Psi_1(a) \right. \\ \left. + \frac{5}{2} a [2\Psi_2(a) + \Psi_0(a)] \right\} \mathbf{N}_2^{-1} , \end{aligned} \quad (12c)$$

$$\begin{aligned} \Delta_3^{-1} = \left\{ \frac{35}{12} \Delta_2 \Delta_1 \Delta_0 \mathbf{M}_3 - \frac{1}{6} [35\Delta_2 + 28\Delta_0] \mathbf{M}_1 + \frac{35}{12} a^3 \Delta_2 \Delta_1 \Psi_1(a) \right. \\ \left. + \frac{35}{12} a^2 \Delta_2 [2\Psi_2(a) + \Psi_0(a)] + 7a \Psi_3(a) \right\} \mathbf{N}_3^{-1} , \end{aligned} \quad (12d)$$

and

$$\begin{aligned} \Delta_4^{-1} = \left\{ \frac{105}{64} \Delta_3 \Delta_2 \Delta_1 \Delta_0 \mathbf{M}_4 - \frac{3}{16} [35\Delta_3 \Delta_2 + 28\Delta_3 \Delta_0 + 27\Delta_1 \Delta_0] \mathbf{M}_2 \right. \\ \left. + \frac{27}{8} \mathbf{M}_0 + \frac{105}{64} a^4 \Delta_3 \Delta_2 \Delta_1 \Psi_1(a) \right. \\ \left. + \frac{35}{16} a^3 \Delta_3 \Delta_2 [2\Psi_2(a) + \Psi_0(a)] \right. \\ \left. + \frac{9}{16} a^2 [14\Delta_3 \Psi_3(a) - 9\Delta_1 \Psi_1(a)] \right. \\ \left. + \frac{9}{8} a [8\Psi_4(a) - 3\Psi_0(a)] \right\} \mathbf{N}_4^{-1} . \end{aligned} \quad (12e)$$

In Eqs. (12), we have used

$$\mathbf{N}_l = (l+1) [\Psi_{l+1}(0) - \Psi_{l+1}(a)] + l [\Psi_{l-1}(0) - \Psi_{l-1}(a)] . \quad (13)$$

### ACKNOWLEDGMENTS

The author is grateful to P. Benoist and to the Centre d'Etudes Nucléaires de Saclay for their kind hospitality and partial support for this work, which was also supported in part by the National Science Foundation grant ENG. 7709405.